

## 全球负荷形变场(时变重力场)球谐综合算法公式

地球表层大气、土壤水、江河湖库水、冰川冰盖雪山、地下水和海平面变化, 都是非潮汐的, 这些地表非潮汐负荷变化可用地面等效水高变化统一表示。地面点 $(R, \theta, \lambda)$ 处等效水高变化 $h_w$ 可表示为规格化负荷球谐级数:

$$h_w(R, \theta, \lambda) = R \sum_{n=1}^{\infty} \sum_{m=0}^n [\Delta C_{nm}^w \cos m\lambda + \Delta S_{nm}^w \sin m\lambda] \bar{P}_{nm}(\cos\theta) \quad (1)$$

式中:  $R$ 为地球平均半径;  $\Delta C_{nm}^w, \Delta S_{nm}^w$ 为 $n$ 阶 $m$ 次规格化负荷球谐系数;  $\bar{P}_{nm}(t) = \bar{P}_{nm}$ 为完全规格化缔合 Legendre 函数。

全球地面等效水高的质量(面密度 $\rho_w h_w$ )分布, 直接引起地面重力位变化:

$$\Phi^d(R, \theta, \lambda) = \sum_{n=1}^{\infty} \frac{4\pi G \rho_w R^2}{2n+1} \sum_{m=0}^n [\Delta C_{nm}^w \cos m\lambda + \Delta S_{nm}^w \sin m\lambda] \bar{P}_{nm} \quad (2)$$

由地球重力场理论可知, 地面重力位变化 $\Phi^d$ 也可用引力位系数变化表示为:

$$\Phi^d = \frac{GM}{R} \sum_{n=1}^{\infty} \sum_{m=0}^n (\Delta \bar{C}_{nm} \cos m\lambda + \Delta \bar{S}_{nm} \sin m\lambda) \bar{P}_{nm}(\cos\theta) \quad (3)$$

式中:  $\Delta \bar{C}_{nm}, \Delta \bar{S}_{nm}$ 为完全规格化的位系数变化。

比较(2)与(3)式, 得:

$$\Delta \bar{C}_{nm} = \frac{4\pi R^3}{M} \frac{\rho_w}{2n+1} \Delta C_{nm}^w = \frac{4\pi R^3}{\rho_e V} \frac{\rho_w}{2n+1} \Delta C_{nm}^w = \frac{4\pi R^3}{4\pi R^3 \rho_e / 3} \frac{\rho_w}{2n+1} \Delta C_{nm}^w = \frac{3}{2n+1} \frac{\rho_w}{\rho_e} \Delta C_{nm}^w$$

$$\text{同理, } \Delta \bar{S}_{nm} = \frac{3}{2n+1} \frac{\rho_w}{\rho_e} \Delta S_{nm}^w \quad (4)$$

式(2)~(4)中,  $G$ 为万有引力常数;  $\rho_w$ 为水的密度;  $\rho_e$ 为地球平均密度;  $M$ 、 $V$ 分别为地球总质量和总体积。

由负荷形变理论可知, 对于地面及固体地球外部,

①高程异常(大地水准面)负荷影响

$$\zeta = \frac{GM}{\gamma r} \sum_{n=2}^{\infty} \left(\frac{a}{r}\right)^n (1 + k'_n) \sum_{m=0}^n (\Delta \bar{C}_{nm} \cos m\lambda + \Delta \bar{S}_{nm} \sin m\lambda) \bar{P}_{nm} \quad (5)$$

②地面重力负荷影响⊙

$$g_t = \frac{GM}{r^2} \sum_{n=2}^{\infty} (n+1) \left(1 + \frac{2}{n} h'_n - \frac{n+1}{n} k'_n\right) \left(\frac{a}{r}\right)^n \sum_{m=0}^n (\Delta \bar{C}_{nm} \cos m\lambda + \Delta \bar{S}_{nm} \sin m\lambda) \bar{P}_{nm} \quad (6)$$

③扰动重力负荷影响

$$\delta g = \frac{GM}{r^2} \sum_{n=2}^{\infty} (n+1) (1 + k'_n) \left(\frac{a}{r}\right)^n \sum_{m=0}^n (\Delta \bar{C}_{nm} \cos m\lambda + \Delta \bar{S}_{nm} \sin m\lambda) \bar{P}_{nm} \quad (7)$$

④地倾斜负荷影响⊙

$$\text{南向: } \xi^s = \frac{GM}{\gamma r^2} \sin \theta \sum_{n=2}^{\infty} (1 + k'_n - h'_n) \left(\frac{a}{r}\right)^n \sum_{m=0}^n (\Delta \bar{C}_{nm} \cos m\lambda + \Delta \bar{S}_{nm} \sin m\lambda) \frac{\partial}{\partial \theta} \bar{P}_{nm} \quad (8)$$

$$\text{西向: } \eta^s = \frac{GM}{\gamma r^2 \sin \theta} \sum_{n=2}^{\infty} (1 + k'_n - h'_n) \left(\frac{a}{r}\right)^n \sum_{m=1}^n m (\Delta \bar{C}_{nm} \sin m\lambda - \Delta \bar{S}_{nm} \cos m\lambda) \bar{P}_{nm} \quad (9)$$

⑤垂线偏差负荷影响

$$\text{南向: } \xi = \frac{GM}{\gamma r^2} \sin \theta \sum_{n=2}^{\infty} (1 + k'_n) \left(\frac{a}{r}\right)^n \sum_{m=0}^n (\Delta \bar{C}_{nm} \cos m\lambda + \Delta \bar{S}_{nm} \sin m\lambda) \frac{\partial}{\partial \theta} \bar{P}_{nm} \quad (10)$$

$$\text{西向: } \eta = \frac{GM}{\gamma r^2 \sin \theta} \sum_{n=2}^{\infty} (1 + k'_n) \left(\frac{a}{r}\right)^n \sum_{m=1}^n m (\Delta \bar{C}_{nm} \sin m\lambda - \Delta \bar{S}_{nm} \cos m\lambda) \bar{P}_{nm} \quad (11)$$

⑥地面站点位移负荷影响⊙

$$\text{东方向: } e = -\frac{GM}{\gamma r^2 \sin \theta} \sum_{n=2}^{\infty} l'_n \left(\frac{a}{r}\right)^n \sum_{m=1}^n m(\Delta \bar{C}_{nm} \sin m\lambda - \Delta \bar{S}_{nm} \cos m\lambda) \bar{P}_{nm} \quad (12)$$

$$\text{北方向: } n = -\frac{GM}{\gamma r^2} \sin \theta \sum_{n=2}^{\infty} l'_n \left(\frac{a}{r}\right)^n \sum_{m=0}^n (\Delta \bar{C}_{nm} \cos m\lambda + \Delta \bar{S}_{nm} \sin m\lambda) \frac{\partial}{\partial \theta} \bar{P}_{nm} \quad (13)$$

$$\text{径向: } r = \frac{GM}{\gamma r} \sum_{n=2}^{\infty} \left(\frac{a}{r}\right)^n h'_n \sum_{m=0}^n (\Delta \bar{C}_{nm} \cos m\lambda + \Delta \bar{S}_{nm} \sin m\lambda) \bar{P}_{nm} \quad (14)$$

⑦扰动重力梯度负荷影响:

$$T_{nn} = -\frac{GM}{r^3} \sum_{n=2}^{\infty} (n+1)(n+2)(1+k'_n) \left(\frac{a}{r}\right)^n \sum_{m=0}^n (\Delta \bar{C}_{nm} \cos m\lambda + \Delta \bar{S}_{nm} \sin m\lambda) \bar{P}_{nm} \quad (15)$$

⑨水平重力梯度负荷影响:

$$\text{北向: } T_{\varphi\varphi} = -\frac{GM}{r^3} \sum_{n=2}^{\infty} (1+k'_n) \left(\frac{a}{r}\right)^n \sum_{m=0}^n (\Delta \bar{C}_{nm} \cos m\lambda + \Delta \bar{S}_{nm} \sin m\lambda) \frac{\partial^2}{\partial \theta^2} \bar{P}_{nm} \quad (16)$$

$$\text{东向: } T_{\lambda\lambda} = -\frac{GM}{r^3 \cos^2 \varphi} \sum_{n=2}^{\infty} (1+k'_n) \left(\frac{a}{r}\right)^n \sum_{m=1}^n (1+k_{nm}) m^2 (\Delta \bar{C}_{nm} \sin m\lambda + \Delta \bar{S}_{nm} \cos m\lambda) \bar{P}_{nm} \quad (17)$$

上述标注⊙的大地测量观测量或参数，只有其点位与地球固连情况下有效。

式 (5) ~ (17) 中  $h'_n$ 、 $l'_n$  和  $k'_n$  分别为  $n$  阶径向、水平和位负荷勒夫数。依据 Farrell 地表负荷形变理论，采用球对称无旋转弹性地球模型 PREM 有关参数，计算地表单位点质量负荷（面密度， $1 \text{ kg/m}^2$ ）作用下的地表负荷勒夫数，如表 1。

表 1 负荷勒夫数取值

阶数 $n$	$h'_n$	$l'_n$	$k'_n$	阶数 $n$	$h'_n$	$l'_n$	$k'_n$
1	-0.2871129880	0.1045044062	-1.0000000000	160	-3.2942117980	0.0058106942	-0.0093636844
2	-0.9945870591	0.0241125159	-0.3057703360	180	-3.3907532400	0.0051551676	-0.0084470364
3	-1.0546530210	0.0708549368	-0.1962722363	200	-3.4867370690	0.0046324760	-0.0077337989
4	-1.0577838950	0.0595872318	-0.1337905897	250	-3.7248624300	0.0037212221	-0.0065109062
5	-1.0911859150	0.0470262750	-0.1047617976	300	-3.9588101480	0.0031642726	-0.0057493979
6	-1.1492536560	0.0394081176	-0.0903495805	350	-4.1853482260	0.0028105951	-0.0052320414
7	-1.2183632010	0.0349940065	-0.0820573391	400	-4.4014325530	0.0025772705	-0.0048534799
8	-1.2904736610	0.0322512320	-0.0765234897	450	-4.6045856190	0.0024162122	-0.0045579733
9	-1.3618478650	0.0303856246	-0.0723928769	500	-4.7931516890	0.0022987082	-0.0043145187
10	-1.4309817610	0.0290225900	-0.0690776844	600	-5.1234075730	0.0021315364	-0.0039191204
12	-1.5609348550	0.0271636708	-0.0638847506	700	-5.3914177940	0.0020034613	-0.0035936423
14	-1.6797703790	0.0259680057	-0.0598385602	800	-5.6025165630	0.0018887552	-0.0033104524
16	-1.7880882500	0.0251266737	-0.0564748883	1000	-5.8875374130	0.0016743075	-0.0028324828

18	-1.8864404740	0.0244708343	-0.0535490132	1500	-6.1543113080	0.0012327687	-0.0020071634
20	-1.9754659020	0.0238986214	-0.0509272630	2000	-6.2038470670	0.0009427101	-0.0015226332
25	-2.1615247260	0.0225448633	-0.0452625739	3000	-6.2137113920	0.0006307787	-0.0010176493
30	-2.3044581340	0.0211578086	-0.0405033192	4000	-6.2144649520	0.0004731032	-0.0007634795
35	-2.4152406280	0.0197609745	-0.0364524519	5000	-6.2148224370	0.0003784752	-0.0006108869
40	-2.5028874800	0.0184188171	-0.0329970228	6000	-6.2150593160	0.0003153917	-0.0005091296
45	-2.5741299450	0.0171690959	-0.0300450548	8000	-6.2153555850	0.0002365398	-0.0003819009
50	-2.6337485520	0.0160264262	-0.0275153569	10000	-6.2155334610	0.0001892299	-0.0003055465
60	-2.7300189390	0.0140651027	-0.0234487653	12000	-6.2156520860	0.0001576905	-0.0002546364
70	-2.8076818590	0.0124702089	-0.0203629907	14000	-6.2157368460	0.0001351626	-0.0002182685
80	-2.8746338100	0.0111640070	-0.0179658948	16000	-6.2158004300	0.0001182669	-0.0001909907
90	-2.9350553590	0.0100800427	-0.0160636283	18000	-6.2158498910	0.0001051258	-0.0001697735
100	-2.9913054190	0.0091686192	-0.0145257169	25000	-6.2159607070	0.0000756901	-0.0001222433
120	-3.0965116190	0.0077267323	-0.0122109806	30000	-6.2160082030	0.0000630749	-0.0001018717
140	-3.1965444360	0.0066448758	-0.0105711243	32000	-6.2160230550	0.0000591327	-0.0000955054
150	-3.2455767690	0.0062018042	-0.0099238838	32768	-6.2160282710	0.0000577468	-0.0000932672
$h'_\infty = -6.209144$			$l'_\infty = 0.000000$			$k'_\infty = 0.000000$	